

Technical Bulletin

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Technical Bulletin #1b

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SHORT SPAN LOAD DESIGN CHART FOR TRANSVERSE HIGH LOAD CONDITIONS

Premier SIPS has completed full scale transverse load testing of our structural building panels at an independent code recognized testing agency. This testing was designed to determine the transverse load carrying capacities of our panels when subjected to extreme load conditions found in roof and floor applications.

Premier SIPS are capable of carrying substantial loads using various methods of connecting the panels; however maximum spans and load carrying capacity are achieved when a double 2x-spline connection is utilized. The detail for this application can be found within the Details Booklet. All panels tested and represented in following Load Design Chart are based on the double 2x connection where all 2x's are continuous through the length of the panel as shown in the details.

Panels with Double 2x's 4' o.c. (Hem-Fir #2)			
EPS Core Thickness	Deflection	4' Span (psf)	8' Span (psf)
3 ½"	L/360	98	45
	L/240	215	67
	L/180	298*	90
5 ½"	L/360	241	128
	L/240	288*	182*
	L/180	288*	182*
7 ¼"	L/360	241	168
	L/240	288*	188*
	L/180	288*	188*
9 ¼"	L/360	274	188*
	L/240	326*	188*
	L/180	326*	188*
11 ¼"	L/360	326*	188*
	L/240	326*	188*
	L/180	326*	188*
* Ultimate load divided by a safety factor of three (3).			
Note: 4' span is a minimum 2 span condition			

Technical Bulletin #2b

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POINT LOAD CONDITIONS ON PANEL WALLS

Premier SIPS panel products are being used in many types of structures as a structural wall. In this application, it is essential to understand the axial capacities of the panel wall and how the load is transferred into a wall panel. In structures where a panel roof system is transferring the roof load to the wall panel, the load transfer is continuous over the length of the wall. Axial capacities found in our load design charts can be utilized as the maximum design loads. However, there are many applications where the load being transferred into a wall panel from the roof or a floor is accomplished through a structural component such as a truss or a beam, which places a point load on the wall panel. Premier Building Systems has conducted full-scale destructive tests at an independent code recognized laboratory to determine the point load capacities for our panel products.

When conducting the tests, it was determined that one of the worst case scenarios the wall panels are subjected to is 2x trusses transferring loads through the narrow edge of the 2x chord onto a 3.5" core panel. Following our typical detail for wall panel installation, a series of tests were conducted to determine the point load capacity of a standard panel. The data from these tests is shown in the chart below. Once values were determined for a standard panel a second series of tests were conducted by the independent laboratory on a standard 3.5" wall that had an additional plate fastened to the top of the panels. This plate can be either standard 2x SPF lumber, 1-1/8" OSB(Oriented Strand Board) or 1-1/8" OSL(Oriented Strand Lumber) i.e. Rimboard, which has been ripped to the overall width of the wall panel so that the OSB skins of the panel are covered by the ripped material. Placement of this additional top plate substantially increases the point load capacity of a panel. The results are shown in the table below.

To calculate the point load that a member will be placing on a panel, it is necessary to take into account the intended live and dead loads and the tributary area that the member is designed to carry. An example would be the placement of roof trusses 2' o.c. which are spanning 60' with only the exterior panel walls as support and the trusses extending 2' beyond the wall for the roof overhang. For this example, let's assume that the live load for the roof is 35 psf and the dead load is 10 psf. In this situation, each truss is placing a point load on the panel wall of 2880 pounds which is in excess of the design point load allowed for standard detailed panels. However, if an additional top plate is used, the loading is acceptable. Another example would be the same roof with a bearing wall running down the center of the structure. In this scenario the panel walls are subjected to a point load of 1530 pounds which falls within the design capacity for a standard detailed panel wall.

Point Load Design Values		
	1 1/2 " Minimum Bearing	3" Minimum Bearing
Standard Detail	2040 lbs	2450 lbs
Additional Top Plate	4030 lbs	4678 lbs
<i>Design loads reflect the ultimate load divided by a safety factor of three (3).</i>		
<i>Loads in excess of the above values require posts under the point load.</i>		
<i>Posts to be designed by an engineer.</i>		

Technical Bulletin #3c

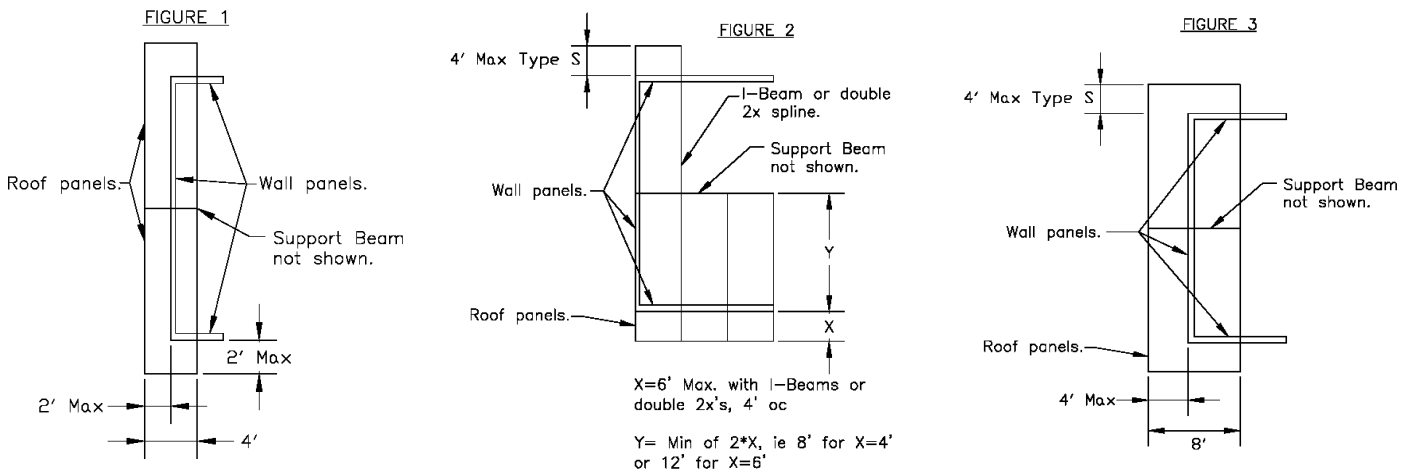
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ROOF PANELS IN CANTILEVER CONDITIONS

Structural Insulated Panels produced by Premier SIPS are used in many applications in which the panel creates the eave and gable end overhangs on a roof. The use of panels to create the overhangs is advantageous because it speeds the construction of the project and saves labor costs associated with hand framing. Some areas of the country use relatively small eaves while other portions of the country prefer larger overhangs. Premier SIPS has had their structural insulated panels evaluated through a series of full scale destructive tests at an independent code recognized laboratory to determine the capabilities of Premier SIPS in cantilever applications. These full scale tests followed ASTM E-72 parameters for loading and monitoring deflection of the tested panels. The following addresses the capabilities of Premier SIPS when installed in a cantilever application for roof overhangs.

When evaluating overhangs or cantilevers consideration must be given as to how the panel is to be used on the roof. The two applications that are possible include having the panel span parallel to the support wall (FIGURE 1 and FIGURE 3) and having the panel span perpendicular to the support wall (FIGURE 2). Panels installed perpendicular to the support wall are capable of supporting greater overhangs.



Premier SIPS used to create overhangs on gable end walls or on eave applications where the panel is parallel to the support wall can be used up to 2' in unsupported overhangs (FIGURE 1). Panels used parallel to the support wall can support loads indicated in the "Cantilevered Roof Panels Parallel to Support Wall - Type "S" Panel Capacity" load chart shown below.

Applications that allow for 8' panel widths may have overhangs of up to 4' when applied parallel as described above (FIGURE 3). Four-foot overhangs of this type have load capacities equal to the loads indicated in the "Cantilevered Roof Panels Parallel to Support Wall - Type "S" Panel Capacity" load chart shown below.

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Standard splined or Type S Panels (detail PBS-005) that are perpendicular to the support wall are capable of supporting 4' horizontal span overhangs provided the panel extends back onto the roof a minimum of twice the distance of the overhang span.

In situations where increased loads are required or where an overhang greater than 4' is desired, Premier SIPS that utilize double 2x's or wood I-beams as the spline mechanism (PBS-006 or PBS-007) can be used. These applications are created when the panels are perpendicular to the support wall and the panels extend back on to the roof to a support, a minimum distance of twice the length of the overhang. When the double 2x or wood I-beams are used at a frequency of 4' o.c., as the attachment spline between panels, overhangs of up to 6' can be achieved.

Greater loads can be achieved if the double 2x's or wood I-beams are used at a frequency of 2' o.c. Overhangs of up to 6' feet of horizontal projection are possible. As stated earlier, the panel assembly must extend back onto the roof, to a support, at a minimum twice the intended overhang horizontal span.

Refer to the load chart "Cantilevered Roof Panels Perpendicular to Support Wall (Figure 2) Panel Capacity", shown below, for load capacities of cantilevered roof panels in these cases.

Cantilevered Roof Panels Parallel to Support Wall - Type "S" Panel Capacity (psf)		
Panel Core Thickness	Figure 1	Figure 2
	2' Maximum Cantilever	4' Maximum Cantilever
3 1/2"	81*	41*
5 1/2"	114*	57*
7 1/4"	149*	75*
9 1/4"	161*	81*
11 1/4"	166*	83*

* Value is less than the ultimate load divided by a safety factor of three.

Cantilevered Roof Panels Perpendicular to Support Wall (Figure 2) Panel Capacity (psf)					
Panel Core Thickness	Type "S" Panel	Type "L" or "I" Panels with Splines 4' o.c.		Type "L" or "I" Panels with Splines 2' o.c.	
	4' cantilever with minimum 8' back span	4' cantilever with minimum 8' back span	6' cantilever with minimum 12' back span	4' cantilever with minimum 8' back span	6' cantilever with minimum 12' back span
3 1/2"	41*	53*	54*	81*	53*
5 1/2"	57*	87*	67*	114*	87*
7 1/4"	75*	115*	84*	149*	115*
9 1/4"	81*	125*	91*	161*	125*
11 1/4"	83*	129*	93*	166*	129*

* Value is less than the ultimate load divided by a safety factor of three.

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WALL PANEL DESIGN LOADS

Building materials that are utilized to create structural components such as walls are subject to a combination of loads. Wall assemblies must be able to withstand axial forces, while at the same time resisting a bending load. Most building materials including concrete, steel lumber and other engineered wood products determine their acceptability for application, in an assembly, through the use of a well-known engineering formula known as the Unity Equation.

The Unity Equation takes into account the ultimate load capacity for a product in both the axial and transverse directions. These ultimate loads are divided by a factor of safety which yields design values. In determining if a product is acceptable for use, the product must meet the following formula:

$$\frac{f_a \text{ (Design Axial Load)}}{F_a \text{ (Allowable Axial Load)}} + \frac{f_b \text{ (Design Bending Load)}}{F_b \text{ (Allowable Bending Load)}} < 1$$

Premier SIPS have undergone extensive testing that allows design professionals to utilize this engineering formula in their work with Premier SIPS. Premier SIPS has the necessary data through full scale destructive testing at independent code recognized laboratories. Attached is a compilation of this data in the form of a Load Design Chart. The chart has been put together with the design axial load listed on top and the design transverse load beneath..

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WALL PANEL ALLOWABLE DESIGN LOADS TYPE S Panels							
Panel Core		8'	10'	12'	16'	20'	24'
3 ½"	Axial Load plf	3500	2553	2452	2118	N/A	N/A
	Trans Load psf	61	57	45	21	N/A	N/A
5 ½"	Axial Load plf	4250	4042	3373	3358	2817	N/A
	Trans Load psf	80	60	46	34	21	N/A
7 ¼"	Axial Load plf	4917	4325	4473	4194	3496	3067
	Trans Load psf	85	75	69	50	31	24
9 ¼"	Axial Load plf	4200	4200	4200	4200	3389	3247
	Trans Load psf	86	65	57	46	39	34
11 ¼"	Axial Load plf	3890	3890	3890	3890	3890	3333
	Trans Load psf	94	76	59	51	39	33
Axial loads represent ultimate divided by a safety factor of 3.							
Transverse loads are less than or equal to L/180 deflection or ultimate load divided by a safety factor of 3.							
Loads do not reflect secondary effect of PΔ.							

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WALL PANEL ALLOWABLE DESIGN LOADS							
TYPE L Panels							
Panel Core		8'	10'	12'	16'	20'	24'
3 ½"	Axial Load plf	4723	3903	3094	2350	N/A	N/A
	Trans Load psf	91	61	45	23	N/A	N/A
5 ½"	Axial Load plf	5849	5889	4278	4311	2933	N/A
	Trans Load psf	182	112	80	49	29	N/A
7 ¼"	Axial Load plf	6850	6111	5556	5181	4835	4082
	Trans Load psf	188	133	117	80	44	24
9 ¼"	Axial Load plf	5470	5470	5470	5470	5470	4250
	Trans Load psf	188	147	134	108	68	53
11 ¼"	Axial Load plf	4500	4333	4167	3750	3750	3333
	Trans Load psf	188	167	153	110	83	70
Axial loads represent ultimate divided by a safety factor of 3.							
Transverse loads are less than or equal to L/180 deflection or ultimate load divided by a safety factor of 3.							
Loads do not reflect secondary effect of PΔ.							
2x's are spaced at 4' on center.							

Technical Bulletin #5b

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STAPLE USE IN PANEL CONNECTIONS

Premier SIPs typically use 8d nails at 6" on center for the connection of splines and plates as shown in the typical details. Many contractors prefer to use staples as the typical fastener for their projects. Staples may be used instead of 8d nails provided they meet the following criteria:

Minimum Staple Length = 1- ½"

14 gauge - 6" on center.

16 gauge - 4" on center.

Chisel point staples are preferred

The suggested size and spacing for the staples is an equivalent to the typical 8d nails. Each project should be reviewed to make sure that the minimum nailing patterns satisfy design conditions. High diaphragm loads may require more fasteners depending on the diaphragm design loads.

Staples are not recommended for use in SIP shear walls in seismic design categories D, E and F.

Technical Bulletin #6c

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PREMIER PANEL FASTENERS

Premier SIPS has completed the development of a panel fastener. This fastener was developed specifically, for the attachment of Premier SIPS to beams, purlins and posts made of wood and soft iron. Premier SIPS panel fastener uses state of the art tempering and coating technology to create a #14 screw that drives easily into wood, engineered woods and soft steel without bending, breaking or stripping out the multi-lobed head. The screw is corrosion resist and passes more than 15 cycles in the industry standard "Kesternich cabinet".

The screw has been designed with an aggressive thread pattern that demonstrates excellent pull out resistance. In independent code recognized laboratory testing, Premier SIPS panel fasteners exhibited 980 pounds of pull-out resistance when installed 1" into a typical SPF#2 2 x 4. The laboratory also checked the screw for resistance to shear. The test was designed to simulate a worst case scenario where a 14" Premier SIPS panel fastener was driven through a 12" thick panel and into SPF#2 dimensional lumber. The fastener withstood over 830 pounds of force without shearing. The failure mode was the screw head pulling through the OSB. The design of the screw head provides a pull-through capacity of 735 pounds. These values are the tested ultimate capacities.

The use of the Premier SIPS panel fastener is specified in the Premier SIPS typical details. Wall connections require that screws be utilized 2' on center. The frequency of panel fasteners required to anchor roof panels is dependent on the imposed loads the panels must resist and the number of attachment points available. See the Premier SIPS typical details for recommendations and follow the requirements specified on the shop drawings.

The Premier SIPS panel fastener can be used in light gauge steel framing up to ¼" thick. Different points are used on the Premier SIPS panel fasteners that are used in these light gauge steel applications, so you will want to check with your Premier SIPS representative for the requirements of your specific project.

Technical Bulletin #7b

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FIRE RESISTIVE ASSEMBLIES

Premier SIPS has conducted the most extensive fire assembly testing in the SIP Industry. As a result of this destructive testing, we can document the performance of Premier SIPS under the rigorous test standards of ASTM – E119, ASTM - E84 and UBC 26-3. One Hour fire resistive assemblies are achieved by combinations of underlying structure and protection of that structure by Gypsum Wall Board.

Residential structures are typically required to meet a fifteen minute standard. That standard is commonly met by applying ½" layer of gypsum drywall over Premier SIPS panels.

Commercial and multi-family structures can be required to meet one-hour fire resistive standards. These prescriptive assemblies are listed in the UL Fire Resistive Assembly Book, but can be summarized as follows;

- 1.) Two layers of 5/8" Type X gypsum, attached per Premier SIPS code report, over Premier SIPS panels with either spline or lumber connections.
- 2.) One layer of 5/8" Type C gypsum, attached per Premier SIPS code report, over Premier SIPS panels joined with dimensional lumber or solid engineered wood products.

As with any fire resistive issue, the local jurisdiction requirements will vary by region. You should contact your local building department to determine requirements and involve the Premier SIPS Sales and Technical team early in the design process in order to satisfy any concerns by either the building department or the design professional.

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WIRING PREMIER SIPS

The Structural Insulated Panels manufactured by Premier SIPS are both simple and easy for electricians to wire. It does require a small amount of advance planning. 1-1/2" diameter wiring chases are provided in the panel cores for quick access by the electricians. The chases are typically located at 16" and 45" off the finished floor as well as vertically 4' on center. These locations as well as any custom chases should be verified during the shop drawing phase.

Type NM-B cable, as labeled by Underwriters Laboratories, passes UL-719 that mandates a maximum conductor temperature of 900°C (1940°F). The conductor temperatures under normal loads will not exceed 600°C, due to the restrictions on amperage loading and breaker sensitivity.

The wiring used for most residential and light commercial structures, commonly referred to as "Romex", is widely available with the NM-B designation labeled by UL and is acceptable for use with Premier SIPS.

Technical Bulletin #9b

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MECHANICAL VENTILATION OF SIP STRUCTURES

As we insulate and seal homes to achieve greater levels of comfort and energy independence, Premier SIPS have proven themselves to be the most cost effective and stable method of construction. Although this simplified process of super-insulation has shown positive impacts on the quality, comfort and energy savings of structures, it has also created the need for controlled ventilation. Many of today's indoor airborne pollutants can be effectively controlled, and ultimately increase the comfort and livability of a structure.

Mechanical ventilation has proven effective in mitigating fumes from combustion appliances, radon, formaldehyde and even pollutants such as excess humidity and tobacco smoke. Established levels of humidity are governed by region. A rough rule of thumb is to limit the relative humidity, in the interior of a building, to 50% or less. This will be low enough to inhibit mold or mildew based pollutants yet high enough to reduce low humidity pollutants like dust mites.

In order to remove the contaminated air, a means of exhaust is essential. Typically, that exhausted air is replaced with fresh air from outside the structure. Several methods of accomplishing this are available. They are listed as follows:

- 1.) Air to air heat exchangers - These small units generally draw air from source areas like kitchens and bathrooms where excess humidity is created. Moisture laden warm air is carried through ducts to the unit where it transfers the heat through a core, similar in function to the radiator of a car, while carrying the moisture out of the structure. Thus, the exhaust air tempers or pre-heats the cold unconditioned but fresh air that is coming in from outside. These units are also known as HRV's or Heat Recovery Ventilators.
- 2.) Exhaust only systems - These units come in many shapes and sizes from, simple one room units to multiple duct whole house exhausts. This type of unit typically exhausts the stale air and relies upon natural infiltration to replace the exhausted air. Exhaust only systems can create a negative pressure in the structure.
- 3.) Ventilating windows - These windows use a small grille to both exhaust and replace air in a house. They are manually operated and can be used in selected windows or in every window in a home.
- 4.) Air Cleaners - These units run the gamut from inexpensive table top versions to very sophisticated whole house systems. They are used to remove particulate pollutants but generally are not designed for the removal of gaseous pollutants. Typically these are not recommended for either humidity or radon control.

Whatever your choice in mechanical ventilation, your design professional should be involved in any indoor air quality maintenance design. Several sources are available for in depth, objective, information on the subject of air quality.

Some are listed below:

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National Center for Appropriate Technology

P.O. Box 2525
Butte, MT 59702-2525
(800) 428-2525

Energy Efficiency and Renewable Energy Clearinghouse

P.O. Box 3048
Merrifield, VA 22116
(800) DOE-EREC



Technical Bulletin #10c

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PREMIER PANEL USED AS HEADERS

When erecting structures that utilize Premier SIPs for the wall assemblies, several options are available to the contractor when a window, door or other opening requires a load to be carried over the opening. Typically, a situation of this type requires a header. Premier SIPs allow the contractor several options that include, Premier's Insulbeam II, using the panel as a header, or the use of conventional materials for the header. Premier's Insulbeam II and the use of the panel as a header are best suited for panel applications since both provide insulation in the header area.

When a header is used, the load carrying capacity of the header must be established and determined acceptable for the intended application. Refer to Premier SIPs load charts for the necessary design information required so a designer, engineer or contractor may determine whether a panel can be used as a header. Current load charts maybe found at www.premiersips.com.

In cases where a concentrated load is placed over an opening or the design loads exceed the capacity of the panel header, Premier's Insulbeam II should be used. If these header options do not work, other engineered header assemblies will need to be considered.

Technical Bulletin #11b

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SCREW FASTENER CAPACITIES IN OSB

In order to finish a project that utilizes Premier SIPS for the walls and roof of the structure, many types of materials need to be fastened to the panels. These materials can include, siding, roofing materials, other structural elements, cabinets, and a host of other items.

In many of these applications screws are the preferred fasteners. Data on the pullout and lateral withdrawal capacities of screws into OSB have not been readily accessible. To help clarify the performance of screws installed in OSB, a major manufacturer of OSB, generated data on various screws installed in OSB. The OSB was exposed to three different environments. Fifteen repetitions of both direct and lateral withdrawal of each screw type, in each of the three environmental conditions were conducted. The following tables summarize the lowest, ultimate average, value achieved for a particular screw type when installed in three different thicknesses of OSB.

AVERAGE DIRECT WITHDRAWAL (PULLOUT) - lbs.			
SCREW SIZE	7/16" OSB	5/8" OSB	3/4" OSB
#6 Deck Screw	177	272	324
#8 Deck Screw	182	309	359
#10 Deck Screw	198	355	363
#12 Roofing Screw	190	312	360
#14 Roofing Screw	177	340	393

These values are ultimate values. Appropriate safety factors should be applied to obtain design values.

AVERAGE LATERAL WITHDRAWAL (SHEAR) - lbs.			
SCREW SIZE	7/16" OSB	5/8" OSB	3/4" OSB
#6 Deck Screw	198	273	295
#8 Deck Screw	118	197	224
#10 Deck Screw	143	260	301
#12 Roofing Screw	436	581	561
#14 Roofing Screw	466	630	797

These values are ultimate values. Appropriate safety factors should be applied to obtain design values.

Technical Bulletin #12b

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NAIL WITHDRAWAL CAPACITIES IN OSB

With the use of Premier SIPS Structural Insulated Panels there are numerous instances where the attachment of finishing materials such as shingles, siding, drywall etc... is required. The application of these materials is typically accomplished through the use of conventional nail products. Data pertaining to the pullout resistance of nails in OSB is not readily available. To provide data on direct withdrawal resistance of nail fasteners placed into the face of Premier SIPS, an independent code recognized testing firm conducted withdrawal tests following standard ASTM D1037 procedures. The following is a summary of the average ultimate values achieved for various nail fasteners placed into 7/16" OSB.

AVERAGE DIRECT WITHDRAWAL (PULLOUT) – lbs.	
NAIL SIZE & DESCRIPTION	AVG. ULTIMATE PULLOUT
4d ring shank-drywall nail	133
6d smooth galvanized	59
Roofing Nail-smooth galvanized	51
8d smooth coated sinker	150
8d smooth galvanized spiral shank	112
8d galvanized ring shank	77
8d smooth galvanized	65
8d bright box	107
10d galvanized ring shank	164
16d smooth galvanized	63
16d bright box	90
These values are ultimate values. Appropriate safety factors should be applied to obtain design values.	

This data has been compiled to provide manufacturers, designers and engineers with values for assessment of fastener requirements.

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PREMIER PANELS WITH I-JOIST'S

In an effort to offer our customers the optimum in energy efficiency, Premier SIPS utilize APA rated I-Joists as an interconnecting spline within our structural insulated panels. Utilizing the I-Joist spline minimizes the thermal short circuiting that may occur with other types of spline options. Premier SIPS has conducted full-scale destructive transverse load testing with an independent code recognized testing laboratory to determine the capacity of our Type I panels for various spans.

The Type I load chart summarizes the panel capacities obtained from full scale destructive testing of Premier SIPS Type I panels. It should be noted that when an I-Joist is used as a spline member it is spaced at a maximum of 4' on center and extends the full length of the panel. See PBS detail PBS-309, in the Premier SIPS typical details. The minimum bearing required to support the panel ends is 1-1/2". In the case of a single span roof panel, spanning from the ridge to the eave, the 2x blocking at the top and bottom of the panel will not be continuous because the I-Joist extends to the panel edges.

Current load charts maybe found at www.premiersips.com.

Technical Bulletin #14d

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PREMIER PANEL MASTIC USAGE

The installation of Premier SIPS utilizes special mastic that has been formulated specifically for use with Premier SIPS. This formulation of mastic consists of polymers that are designed to remain flexible and provide a seal against water vapor transmission and air infiltration. Although Premier SIPS Panel Mastic has slight, intrinsic, adhesive properties, it should be noted that all of Premier SIPS structural testing has been conducted without the mastic in place.

Premier SIPS Panel Mastic is used in conjunction with Premier SIPS at various locations including bottom plate placement, all foam to foam interfaces, foam to wood interfaces such as top and bottom plate placement and all wood to wood interfaces. The attached chart has taken into account the use of Premier SIPS Panel Mastic in these various areas and will provide you a basis for estimating the amount of mastic required for your Premier SIPS project. Note that the chart has been developed using a 3/8" diameter bead on all foam to foam and wood to foam interfaces and a 3/16" diameter bead for wood to wood interfaces. This means that each joint will typically have 1-3/8" diameter bead and 2-3/16" diameter beads of mastic per foot of panel edge. Allow for waste and other factors when estimating mastic quantities.

ESTIMATING CHART for PREMIER PANEL MASTIC	
Panel Size	Amount of Premier Panel Mastic 28 oz. tube
4' x 8'	0.94
4' x 10'	1.10
4' x 12'	1.26
4' x 14'	1.42
4' x 16'	1.57
4' x 18'	1.73
4' x 20'	1.89
4' x 22'	2.05
4' x 24'	2.20
8' x 8'	1.26
8' x 10'	1.42
8' x 12'	1.57
8' x 14'	1.73
8' x 16'	1.89
8' x 18'	2.05
8' x 20'	2.20
8' x 22'	2.36
8' x 24'	2.52

Technical Bulletin #15c

Created: 3-17-99, Revised: 6-15-11



WIND SPEED VS. PRESSURE

The building codes have set forth minimum design criteria that must be met when structurally designing a building. These criteria are for both gravity and lateral loading. The purpose of this technical bulletin is to touch on the requirements for designing structures to resist wind loads.

Both the IRC and the IBC reference ASCE 7 to determine design wind pressures for a structure. ASCE 7 has three methods for determining wind loads on structures. This technical bulletin uses the simplified procedure to create the following chart as an aide in estimating a structures design wind load requirements. This chart is not intended to be used for the final structural design of the structure. Your design professional will need to determine the final design for your specific project.

Wall Loads (psf) - End Zone (Zone 5) for 100sf to 500 sf effective wind area												
Mean Roof Height (ft)	90 MPH			100 MPH			110 MPH			120 MPH		
	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D
15	-15.1	-18.3	-22.2	-18.7	-22.6	-27.5	-22.6	-27.3	-33.2	-26.9	-32.5	-39.5
20	-15.1	-19.5	-23.4	-18.7	-24.1	-29.0	-22.6	-29.2	-35.0	-26.9	-34.7	-41.7
25	-15.1	-20.4	-24.3	-18.7	-25.2	-30.1	-22.6	-30.5	-36.4	-26.9	-36.3	-43.3
30	-15.1	-21.1	-25.1	-18.7	-26.2	-31.0	-22.6	-31.6	-37.5	-26.9	-37.7	-44.7
35	-15.9	-21.9	-25.7	-19.6	-27.1	-31.8	-23.7	-32.8	-38.4	-28.2	-39.0	-45.7
40	-16.5	-22.5	-26.3	-20.4	-27.9	-32.5	-24.6	-33.7	-39.3	-29.3	-40.1	-46.8
45	-16.9	-23.1	-26.9	-20.9	-28.6	-33.3	-25.3	-34.6	-40.2	-30.1	-41.2	-47.9
50	-17.5	-23.6	-27.3	-21.7	-29.2	-33.8	-26.2	-35.3	-40.9	-31.2	-42.0	-48.7
55	-18.0	-24.0	-27.8	-22.3	-29.7	-34.4	-26.9	-35.9	-41.6	-32.0	-42.8	-49.5
60	-18.4	-24.5	-28.2	-22.8	-30.3	-35.0	-27.6	-36.6	-42.3	-32.8	-43.6	-50.3
Net Design wind pressure	-15.1			-18.7			-22.6			-26.9		

Wall Loads (psf) - End Zone (Zone 5) for 100sf to 500sf effective wind area												
Mean Roof Height (ft)	130 MPH			140 MPH			150 MPH			170 MPH		
	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D	Exp B	Exp C	Exp D
15	-31.6	-38.2	-46.5	-36.7	-44.4	-53.9	-42.1	-50.9	-61.9	-54.1	-65.5	-79.5
20	-31.6	-40.8	-49.0	-36.7	-47.3	-56.9	-42.1	-54.3	-65.3	-54.1	-69.8	-83.9
25	-31.6	-42.7	-50.9	-36.7	-49.5	-59.1	-42.1	-56.8	-67.8	-54.1	-73.0	-87.1
30	-31.6	-44.2	-52.5	-36.7	-51.4	-60.9	-42.1	-58.9	-69.9	-54.1	-75.7	-89.8
35	-33.2	-45.8	-53.7	-38.5	-53.2	-62.4	-44.2	-61.0	-71.6	-56.8	-78.4	-92.0
40	-34.4	-47.1	-55.0	-40.0	-54.7	-63.9	-45.9	-62.7	-73.3	-59.0	-80.6	-94.1
45	-35.4	-48.3	-56.2	-41.1	-56.2	-65.3	-47.2	-64.4	-74.9	-60.6	-82.8	-96.3
50	-36.7	-49.3	-57.2	-42.6	-57.3	-66.4	-48.8	-65.7	-76.2	-62.8	-84.4	-97.9
55	-37.6	-50.2	-58.1	-43.7	-58.4	-67.5	-50.1	-66.9	-77.5	-64.4	-86.0	-99.5
60	-38.6	-51.2	-59.1	-44.8	-59.5	-68.6	-51.4	-68.2	-78.7	-66.0	-87.6	-101.2
Net Design wind pressure	-31.6			-36.7			-42.1			-54.1		

Technical Bulletin #16c

Created: 3-17-99, Revised: 6-15-11



PREMIER SIPS & OFF-GASSING

Premier SIPS Structural Insulated Panels have been used in numerous applications where chemical sensitivity is a consideration. A common question that was asked in these application was “Do the panels emit any harmful gases such as formaldehyde?”

In an effort to definitively answer this question, Premier SIPS contracted with an independent, accredited testing laboratory to conduct formaldehyde testing. ASTM E1333, “Standard Test Method for Determining Formaldehyde Concentrations in Air and Emissions Rates from Wood Products Using a Large Chamber, Standard Face and Back Configuration” was conducted to determine, if in fact, any off gassing does occur. This ASTM test procedure is designed to measure the formaldehyde concentration in air based on the emission rate of newly manufactured products under conditions designed to simulate product use.

The sophisticated test equipment used to measure concentration levels in this test allow detection of emissions down to .03 ppm (parts per million). The result of Premier SIPS in this rigorous test for the formaldehyde concentration in the test chamber was “**Below Minimum Detectable Level**”.

This full scale testing of Premier SIPS demonstrates that Premier SIPS do not emit detectable amounts of formaldehyde.

One must realize that formaldehyde is found in nature and around us, all the time. Plywood and OSB are not going to cause most people any sensitivity problems. Major sources of formaldehyde typically found in the home are from particle board or pressed wood used in furniture, cabinets and shelving and carpeting.

Chemically sensitive individuals have occupied homes utilizing Premier SIPS and have had no reactions what so ever.

Technical Bulletin #17b

Created: 3-17-99, Revised: 6-15-11



RECESSED LIGHTS IN PREMIER SIPS

Premier SIPS are frequently used in vaulted roof/ceiling applications. While the panels provide an excellent method to create a vaulted ceiling, there are limitations on the types of lighting that can be utilized with our panels. The biggest limitation is for recessed or can lights that are intended to be recessed into the finished ceiling and create a flush finish.

Premier SIPS has researched the application of recessed light fixtures and has determined that the application of these type lights into our roof panels could cause problems. These potential problems stem from the heat created by these fixtures and the reduction of panel insulation, which may lead to condensation issues. Premier SIPS recommends that track lighting or some other type of surface mounted lighting be used in lieu of recessed fixtures when Premier SIPS make up the roof/ceiling assembly.

Technical Bulletin #18c

Created: 3-30-99, Revised: 6-15-11



TYPE S PANEL CAPACITIES

In an effort to offer our customers the optimum in energy efficiency, Premier SIPS utilizes the Premier SIPS spline as an interconnecting spline within our structural insulated panels. Utilizing the Premier SIPS spline virtually eliminates the thermal short circuiting that may occur with other types of spline options. To determine the capacities of Type S panels, Premier SIPS has conducted full-scale destructive transverse load testing with a major university and an independent code recognized laboratory.

The Type S load chart summarizes the panel capacities obtained from full scale destructive testing of Premier SIPS Type S panels. The minimum bearing that is required to support the panel end is 1-½". Loads indicated in the load chart for spans greater than limited for floors and roofs are used for wall design.

Current load charts maybe found at www.premiersips.com.

Technical Bulletin #19c

Created: 3-31-99, Revised: 6-15-11



TYPE L PANEL CAPACITIES

Premier SIPS utilizes Type L panels when the structural design loads exceed the capacities of our standard Type S and Type I panels. Details PBS-308 and PBS-007, found in the typical details, depict the Type L panel and connection. The double 2x's used, as the spline mechanism, must extend the full length of the panel. Premier SIPS has conducted full-scale destructive transverse load testing with an independent code recognized testing laboratory to determine the capacity of our Type L panels for various spans.

The Type L load chart summarizes the panel capacities obtained from full scale destructive testing of Premier SIPS Type L panels. When Type L panels are utilized, the maximum spacing of the lumber spline is 4' on center. The minimum bearing that is required to support the panel end is 1-1/2". Loads indicated in the load chart for spans greater than limited for floors and roofs are used for wall design.

Current load charts maybe found at www.premiersips.com.

Technical Bulletin #20b

Created: 4-8-99, Revised: 6-15-11



PREMIER SIPS SPLINES

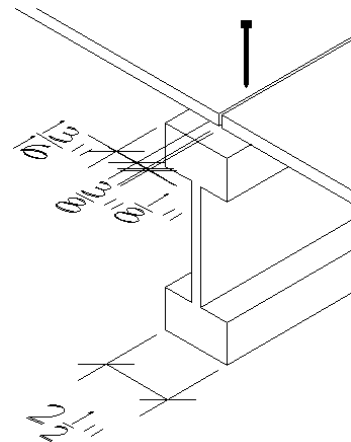
Premier SIPS uses three types of splines for connecting its structural insulated panels. The three types of splines are the Premier SIPS spline for our Type “S” panel, the I-Joist spline for our Type “I” panel and the double 2x or dimensional lumber spline for our Type “L” panel. Each of these splines provides a minimum width for fastening of 3”. These splines and the corresponding minimum width for fastening have been determined with regard to the OSB manufacturers recommended edge fastening distances and what is practical in actual on site conditions.

OSB manufacturers recommend that the minimum edge fastening distance be between $\frac{3}{8}$ ” and $\frac{1}{2}$ ”. When fastening two panels together at a spline joint, the minimum width of spline can be calculated as follows:

- $\frac{1}{2}$ ” edge distance of spline to fastener
- $\frac{3}{8}$ ” edge distance of fastener to OSB
- $\frac{1}{8}$ ” gap in the OSB edges (recommended by OSB mfg.)
- $\frac{3}{8}$ ” edge distance of fastener to OSB
- $\frac{1}{2}$ ” edge distance of spline to fastener

Total = $1 \frac{7}{8}$ ” minimum width of spline

This minimum width for the spline does not allow any wiggle room for the fasteners deviating from the theoretical edge distances. From a practical standpoint, one must realize that pneumatic nailing guns are used to install the fasteners. The accuracy with which one can hit this theoretical line is suspect. From a practical application stand point, Premier SIPS realizes the limitations inherent in the field and chooses to provide more than just the minimum width for our splines. This is also the reason that Premier SIPS does not endorse the use of a single 2x, or any member that is less than $2 \frac{1}{2}$ ” wide, as an acceptable spline member.



Technical Bulletin #21b

Created: 4-8-99, Revised: 6-15-11



PREMIER SIPS PANELS USED IN FLOOR APPLICATIONS

Premier SIPS are often used in floor applications when an insulated floor system is required. Examples of this situation are over a crawl space, the floor of a sun room addition or the bedroom floor over an unheated garage.

When using Premier SIPS in floor applications, there are a few design considerations to keep in mind. Premier SIPS recommends that the floor panel be overlaid with an additional layer of 7/16" sheathing. The reason for this is that in most situations we use 7/16" OSB for the panel skins and we want to minimize puncturing of the panel skins.

Floor panels are not able to support load bearing walls and the floor panels cannot be cantilevered over a lower wall to support upper wall and roof systems.

The load limitations of the panels used in floor systems is covered by our load design charts and other technical bulletins.

Technical Bulletin #22c

Created: 4-26-99, Revised: 6-15-11



DIAPHRAGM CAPACITY OF PREMIER SIPS

Premier SIPS has completed a series of full-scale diaphragm tests to determine design values for Premier SIPS Structural Insulated Panels. These full-scale tests were conducted following the protocols of ASTM E455 “Standard Method for Static Load Testing of Framed Floor or Roof Diaphragm Constructions for Buildings” and ASTM E1803 “Standard Test Methods for Structural Capacities of Insulated Panels”.

Three separate assemblies using variations of fasteners were tested in sets of two, as is required in the ASTM protocols. Each diaphragm was made up of 6-4'x12'x6" panels creating a diaphragm of 8' x 36' for an aspect ratio of 4.5 to 1. The panels were supported on 4x6's at each 8' edge and at the third points along the 36' length of the diaphragm. Along the 36' lengths of the diaphragm were 4x6's that were spliced together to act as the chord members of the diaphragm. The two 8' ends of the diaphragm were the support locations, which simulated shear walls supporting the diaphragm.

The lateral loads were applied to the diaphragm at the third points via a hydraulic ram. The 4x6 frame had reaction points at the end of each of the 8' sides. By applying loads through the panel diaphragm in this manner and having the reaction points on the 4x6 frame, we were assured that the load was applied to the panel diaphragm; therefore, the screw fasteners had to transfer the shear forces to the supporting 4x6's.

Each set of the three panel assemblies varied the number of screws and nails that were used to connect the panels to each other and to the supporting 4x6's. In two of the tests the fastening pattern within the diaphragm varied according to the expected shear forces in the diaphragm. These two diaphragms were sectioned into thirds. The center third of the diaphragm had less fasteners than the outside thirds as the loads in this area are minimal. Fastener number and placement corresponded to the shear diagram of the tested diaphragm, i.e. more fasteners at a closer spacing were used in the outside thirds of the diaphragms as compared to the center third of the diaphragm. Shear is always the greatest at the supported edges. This was done as a means to economize labor as well as the number of fasteners used in the diaphragm. All fasteners installed in these tests were applied on the topside of the diaphragm only. Premier SIPS typical details call for 8d nails at the splines on both faces of the panel. When top spline only methods are used the fastening frequency is doubled.

The first assembly used 8d nails @ 3" on center throughout the diaphragm to fasten the 7/16" OSB splines. The 3" on center spacing was used because the diaphragm was only nailed on the topside. The typical nail spacing is 6" on center for fastening splines on both faces of the panels. The panel screw fasteners were spaced at 12" on center into all of the 4x6's. This diaphragm achieved 450-plf design shear capacity. This value reflects a safety factor of three. The deflection of the diaphragm across the 36' at 435-plf was 0.41".

The second assembly used 8d nails @ 3" on center to fasten the OSB splines in the center third of the diaphragm and 2" on center in the outside thirds. The panel fastener spacing in the outside thirds of the diaphragm was decreased to 3" on center. The screw spacing was changed for the end of the diaphragm as well as along the top and bottom chords of the diaphragm. This diaphragm achieved 550-plf design shear capacity. Again this value has a safety factor of three. The deflection of the diaphragm across the 36' at 538-plf was 0.37".

Technical Bulletin #22c

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The third assembly used 8d nails @ 3" on center to fasten the OSB splines in the center third of the diaphragm and 1 ½" on center in the outside thirds. The panel fastener spacing in the outside thirds of the diaphragm was decreased to 2" on center. The screw spacing was changed for the end of the diaphragm as well as along the top and bottom chords of the diaphragm. This diaphragm had a design value of 750-plf. This value represents a safety factor of three. The deflection of the diaphragm across the 36' at 750-plf was 0.37".

Subsequent to the diaphragm testing just described, Premier SIPS conducted an additional two diaphragm tests. In these tests the same nail and panel fastener spacing was maintained throughout the diaphragm, which consisted of 6-4'x8'x6" panels configured to make an 8'x24' diaphragm.

The first diaphragm utilized 7/16" splines connecting the panels with a nailing pattern of two rows of 0.113" x 2-3/8" nails at 3" on center. Only the top OSB skin was nailed. The perimeter panel fastener screws attaching the diaphragm to the chord members were spaced at 4" on center. This diaphragm had a capacity of 917 plf. The deflection of the diaphragm across the 24' at 917-plf was 0.18".

The second diaphragm utilized 23/32" splines connecting the panels with a nailing pattern of two rows of 0.113" x 2-3/8" nails at 3" on center. Only the top OSB skin was nailed. The perimeter panel fastener screws attaching the diaphragm to the chord members were spaced at 4" on center. This diaphragm had a capacity of 1136 plf. The deflection of the diaphragm across the 24' at 1136-plf was 0.19".

Each of the values reported for the capacity of the diaphragm is a design value. It has a factor of safety of three associated with it.

In any designs using the diaphragm capacity of the panels, it is up to the designer or engineer to determine the required diaphragm capacities and then apply the values described in this technical bulletin appropriately.

Technical Bulletin #23b

Created: 12-4-99, Revised: 6-15-11



COMBUSTION TOXICITY OF PREMIER SIPS

Premier SIPS have undergone numerous fire tests for code recognition of our panels including ASTM E84 “Surface Burning Characteristics”, ASTM E119 “Hourly Testing” UL 1715 “Corner Room Burn” etc. Panels that have been in real life fire scenarios have also shown that panels hold up well in these events. However, the question regarding gasses that are produced during combustion still arises from time to time.

One must realize that when a material is burned, combustion gases are given off. In the case of Premier SIPS the primary gases given off are carbon monoxide, carbon dioxide and water vapor. These gases are found in many fires containing organic materials. These particular gases are around us all the time. In high concentrations or in the absence of oxygen asphyxiation can occur.

In fires the materials that compose the interior of the structure i.e. carpet, furniture etc. are the primary threat when considering toxic combustion gases. Premier SIPS, when burned, give off by products that are similar to those found when wood is burned.

The building codes have evaluated Premier SIPS and the panels have been found to meet the building codes criteria, which includes fire testing. In addition, our extensive fire testing allows Premier SIPS to carry the mark of Underwriters Laboratories Inc.

Technical Bulletin #24b

Created: 1-12-00, Revised: 6-15-11



ATTACHMENT OF EXTERIOR CLADDINGS TO PREMIER SIPS

Premier SIPS are used in both commercial and residential applications. Through the years our panels have had nearly every type of exterior cladding applied to the face of the panels. The advent of new exterior claddings in the market place always brings the question of how the new product should be applied to the panel. This bulletin is a review of common claddings that are available and their attachment to panels.

Most exterior claddings, currently available in the market place, make reference that their product should be attached to the framing members of the structure. Premier SIPS do not incorporate framing members and therefore do not meet their written recommendations. A review of the requirements for attachment of the siding material typically calls out for the cladding to be attached with 8d nails 16" or 24" on center depending on the framing spacing. Using these values one can compare the pullout values for 8d nails into standard framing with the fastener pullout values listed in Technical Bulletins #11 and #12. This comparison shows that all claddings with the requirements of fastening to framing members can be matched by applying 8d ring shank nails 12" o.c. into Premier SIPS. This would include the attachment of standard sidings such as hardboard, cedar, redwood, composites and cementations sidings.

This type of comparison is also valid for the application of lath for stucco as well as brick tie placement. Typically, these products are attached to Premier SIPS by simply increasing the number of fasteners 25%. When a manufacturer calls out for fasteners 16" o.c. the fasteners would be placed in a Premier SIPS panel at a spacing of 12" o.c. This will allow the panel application to meet or exceed the pull out values required by the siding manufacturer. It should be noted that the fastener placement can be maintained at the siding manufacturer's recommendations provided a nail/staple is replaced with a screw. In all cases the fastener should be corrosion resistant.

Technical Bulletin #25b

Created: 5-1-03, Revised: 6-15-11



SOUND TRANSMISSION

Premier SIPS have had panels erected in numerous residential and commercial applications where the customers have expressed great satisfaction with the reduced noise level within their structure due to the new construction. While these stories are anecdotal they indicate that structures built with Premier SIPS panels do provide a measure of sound attenuation.

Within the building industry, specific tests are used to determine the Sound Transmission Coefficient (STC)-ASTM E90 of an assembly or component. These tests subject a wall assembly to random noises in a frequency range of 125 Hz – 4000 Hz. The following are STC values for several Premier SIPS panel assemblies used in standard construction, which were determined through testing at a code recognized independent laboratory. These assemblies are for typical residential applications:

Premier SIPS Panel (no finish either face)	STC- 22
½" gyp, Premier SIPS Panel, no finish on other face	STC- 28
5/8" gyp, Premier SIPS Panel, no finish on other face	STC- 29
5/8" gyp, Premier SIPS Panel, 5/8" gyp	STC- 33
2-layers 5/8" gyp, Premier SIPS Panel, 2-layers 5/8" gyp	STC- 41

Premier SIPS panels are also used in town homes and condominiums. Hence, Premier SIPS has also conducted ASTM E90 tests on wall assemblies that produce higher sound attenuation while meeting fire and clearance requirements for these types of structures. These include:

Double Wall Assembly-A 5/8" gyp, Premier SIPS panel, 5/8" gyp, 1" air space, 5/8" gyp, Premier SIPS panel, 5/8" gyp	STC-45
Double Wall Assembly-B 2 layers 5/8" gyp, Premier SIPS panel, 5/8" gyp, 1" air space, 5/8" gyp, Premier SIPS panel, 5/8" gyp	STC-47
Double Wall Assembly-C 2 layers 5/8" gyp, Premier SIPS panel, 5/8" gyp, 1" air space, 5/8" gyp, Premier SIPS panel, 2 layers 5/8" gyp	STC-52
Double Wall Assembly-D 2 layers 5/8" gyp, Premier SIPS panel, 2 layers 5/8" gyp, 1" air space, 5/8" gyp, Premier SIPS panel, 2 layers 5/8" gyp	STC-54

In all cases gypsum wallboard was attached, using standard screws, directly into the face of the panel. In multiple layer applications the joints were offset a minimum of six inches from the joints in the previous layer. The above results will be affected by the use of additional or different finish materials and are supplied as a reference value. It should also be noted that sound attenuation is dependent on installation practices. Electrical penetrations, plumbing and fenestration all can affect the sound transmission performance of a wall assembly.

Technical Bulletin #26b

Created: 5-29-03, Revised: 6-15-11

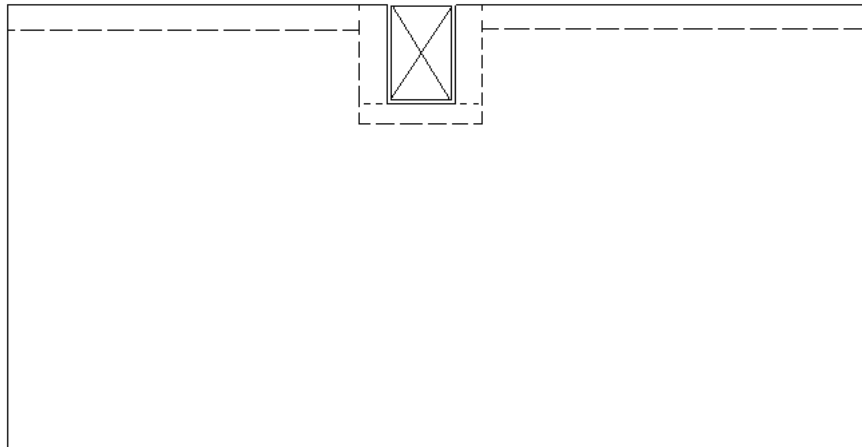


BEAM POCKETS IN PREMIER SIPS

Premier SIPS used in residential construction have had great success especially in the western United States. A design that is favored in these locations calls for beams to be pocketed into the wall panel assembly. This detail provides for an aesthetically pleasing interface between the wall and the support mechanism for roofs and floors.

When this detail is used in conjunction with Premier SIPS the following points should be considered:

- Loads for the type of detail shown below are limited to the point loads established in the Premier SIPS Design Manual. Basically this calls for a maximum design load of 2450 pounds for a standard 2x plate used in the panel under the beam. The use of a cap plate does not allow for increased loads in this application. When loads exceed 2450 pounds posting is required under the beam.
- This detail provides for a thermal short circuit in the wall panel system. Great care should be taken to seal this joint. After sealants are placed in the pocket all interior interfaces must be further sealed with Premier SIPS SIP Tape.
- Maximum design loads can be compromised if the beam pocket is over cut at the corner of the pocket. Good craftsmanship is required to assure that the pocket is not over cut in the corners.



Technical Bulletin #27b

Created: 3-30-07, Revised: 6-15-11



VENTING OF PREMIER SIPS ROOF PANELS

Even though Premier SIPS have been used in unvented roof applications since the 1960's, confusion still exists about the need to vent Premier SIPS roof panels.

The building codes require ventilation of “enclosed attics and enclosed rafter spaces formed where ceilings are applied directly to the underside of roof rafters.” The building code defines an attic as the unfinished space between the ceiling joists of the top story and the roof rafters. When roof panels are used on a project an attic space is not present because the panels are the exterior, insulated envelope of the structure. By definition, an attic space does not exist.

The IRC Section R806.4 furthers the discussion by addressing “unvented conditioned attic assemblies (spaces between the ceiling joists of the top story and the roof rafters)...” But, again, when panels are used on the roof, an attic is not present. The interior space of the structure is all conditioned and usable.

To summarize, roof venting of Premier SIPS roof panels is not required. Refer to Premier SIPS Technical Bulletin #9 for mechanical ventilation of SIP structures.

Technical Bulletin #28d

Created: 5-23-07, Revised: 6-15-11



VAPOR RETARDERS WITH PREMIER SIPS RESIDENTIAL PANELS

Questions about using vapor retarders in conjunction with Premier SIPS structural insulated floor, wall and roof panels come up often. When installing Premier SIPS panels, Premier SIPS requires the proper application (as shown in the Premier SIPS Typical Details) of panel mastic at all panel joints. The function of the mastic is to provide a seal against water vapor transmission and air infiltration.

The purpose of this technical bulletin is to provide guidelines for the use of vapor retarders with Premier SIPS in residential applications.

The International Residential Code (IRC) requires the following:

SECTION R318 - MOISTURE VAPOR RETARDERS

R318.1 Moisture control: In all framed walls, floors and roof/ceilings comprising elements of the building thermal envelope, a vapor retarder shall be installed on the warm-in-winter side of the insulation.

Exceptions:

1. In construction where moisture or freezing will not damage the materials.
2. Where the framed cavity or space is ventilated to allow moisture to escape.
3. In counties identified as in climate zones 1 through 4 in Table N1101.2.

The definition of a vapor retarder, from the IRC is:

VAPOR RETARDER: A vapor resistant material, membrane or covering such as foil, plastic sheeting, or insulation facing having a permeance rating of 1 perm or less, when tested in accordance with the desiccant method using Procedure A of ASTM E96. Vapor retarders limit the amount of moisture vapor that passes through a material or wall assembly.

The APA has determined that OSB has a perm rating of less than 1. Since the OSB skins, of the panels that Premier SIPS produces, have a permeance rating of less than 1, the panel joint is the primary area of concern with a SIP system when considering vapor retarder application. Premier SIPS requires that panel mastic be used when joining panels. Premier SIPS also recommends the use of SIP Tape over the panel joints. The SIP Tape is formulated with a permeance of less than 1. The combination of the OSB skins and the SIP Tape meets the building code requirements for vapor retarders.

Typically, 6" wide SIP Tape is used at all wall and roof panel joints as well as at wall panel corners. The connection of roof panels to exterior wall panels requires the use of 12" wide SIP Tape.

Roof panels that have joints on supporting beams require 18" wide SIP Tape. A ridge beam is an example of this condition.

Technical Bulletin #28d

Created: 5-23-07, Revised: 6-15-11



The use of an additional vapor retarder, such as polyethylene sheeting, maybe warranted based on the local building code and or climatic conditions. It is up to the design professional to make this determination. If an additional vapor retarder is utilized, it must be installed properly.

Please refer to the Premier SIPS typical details for illustrations of these conditions. The typical details can be requested by calling the number below, or it can be viewed online at www.premiersips.com.

Technical Bulletin #29c

Created: 8-28-07, Revised: 6-16-11



PREMIER SIPS USED AS EXTERIOR WALLS

There are numerous opinions about which house wrap or felt, if any, to use on Premier SIPS wall panels. The purpose of this technical bulletin is to provide guidelines for the use of materials over the exterior of Premier SIPS wall panels.

Premier SIPS evaluation report states:

“The exterior face of wall panels are required to be covered with a wall covering, complying with the applicable code or recognized in a current ICC-ES evaluation report. A water-resistive barrier must be installed over the panels in accordance with IBC Section 1404.2, IRC Section R703.2, BNBC Section 1406.3.6, and UBC Section 1402, as applicable, prior to application of the wall covering. Where Portland cement plaster is used, compliance with IBC Sections 2510 and 2512, IRC Section R703.6.3 or UBC Section 2506.4, as applicable, is necessary. All exterior panel joints must be sealed with a compatible acrylic latex caulk.”

Premier SIPS recommends that a water resistive barrier, as recognized by ICC-ES, be installed over Premier SIPS used as exterior walls.

Current ICC-ES Report holders for water-resistive barriers can be obtained by visiting the ICC-ES website at www.icc-es.org and navigating to Evaluation Reports, CSI List, Section 0728 – Water-Resistive Barriers.

The 2006 versions of the IRC and the IBC have the following requirements.

The 2006 International Residential Code (IRC) requires the following:

SECTION R703 – EXTERIOR COVERING

R703.1 General: Exterior walls shall provide the building with a weather-resistant exterior wall envelope. The exterior wall envelope shall include flashing as described in Section R703.8. The exterior wall envelope shall be designed and constructed in a manner that prevents the accumulation of water within the wall assembly by providing a water-resistant barrier behind the exterior veneer as required by Section R703.2 and a means of draining water that enters the assembly to the exterior.

R703.2 Water-resistive barrier: One layer of No. 15 asphalt felt, free from holes and breaks, complying with ASTM D226 for Type 1 felt or other approved water-resistive barrier shall be applied over studs or sheathing of all exterior walls.....

The 2006 International Building Code (IBC) requires the following:

SECTION 1403 – PERFORMANCE REQUIREMENTS

1403.2 Weather protection: Exterior walls shall provide the building with a weather-resistant exterior wall envelope. The exterior wall envelope shall include flashing, as described in Section 1405.3. The exterior wall envelope shall be designed and constructed in such a

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manner as to prevent the accumulation of water within the wall assembly by providing a water-resistant barrier behind the exterior veneer, as described in Section 1404.2, and a means for draining water that enters the assembly to the exterior.

1404.2 Water-resistive barrier: A minimum of one layer of No. 15 asphalt felt, complying with ASTM D226 for Type 1 felt or other approved materials, shall be attached to the studs or sheathing, with flashing as described in Section 1405.3, in such a manner as to provide a continuous water-resistive barrier behind the exterior wall veneer.

The definition of a water-resistive barrier, from the IRC and the IBC is:

WATER-RESISTIVE BARRIER: A material behind an exterior wall covering that is intended to resist liquid water that has penetrated behind the exterior covering from further intruding into the exterior wall assembly.

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HEADERS IN PREMIER SIPS WALL PANELS

Premier SIPS Technical Bulletin #10 addresses the load carrying capacity of Premier SIPS used as headers and refers to the Insul-Beam header. This Technical Bulletin focuses on how to support Insul-Beam headers as well as headers constructed from an engineered wood product like LVL's or built up headers constructed from multiple plies of dimensional lumber.

Many design professionals and builders are familiar with how headers work in conventional framing when considering load distribution around openings. Premier SIPS act differently than conventional stick framing when load paths are considered. Premier SIPS wall panels, typically, do not use dimensional lumber in the panels to transfer gravity loads. The OSB skins are the load transferring elements. It is for this reason that Premier SIPS requires that the OSB skins of the wall panels be completely supported.

In situations where headers, other than Premier SIPS are used, the headers are sandwiched between the OSB faces of the Premier SIPS wall panel. If the header were to be placed directly above the opening, as typically done with stick construction, the only way for gravity loads to transfer to the header from the wall panel OSB faces is through shear transfer of the nails that connect the OSB faces to the header. This situation is acceptable provided it is engineered by a design professional.

For typical situations, Premier SIPS requires the built up headers be placed directly beneath the top plate of the wall and the trimmer studs extend up to the underside of the header. King studs are then added and attached to the trimmer studs as required by the structural design. By using this methodology, the built up header transfers the gravity loads to the trimmer studs through bearing and the wall panel below the header transfers the wind loading to the king studs attached to the trimmer studs. Detail PBS-201 shows this configuration for a wall.

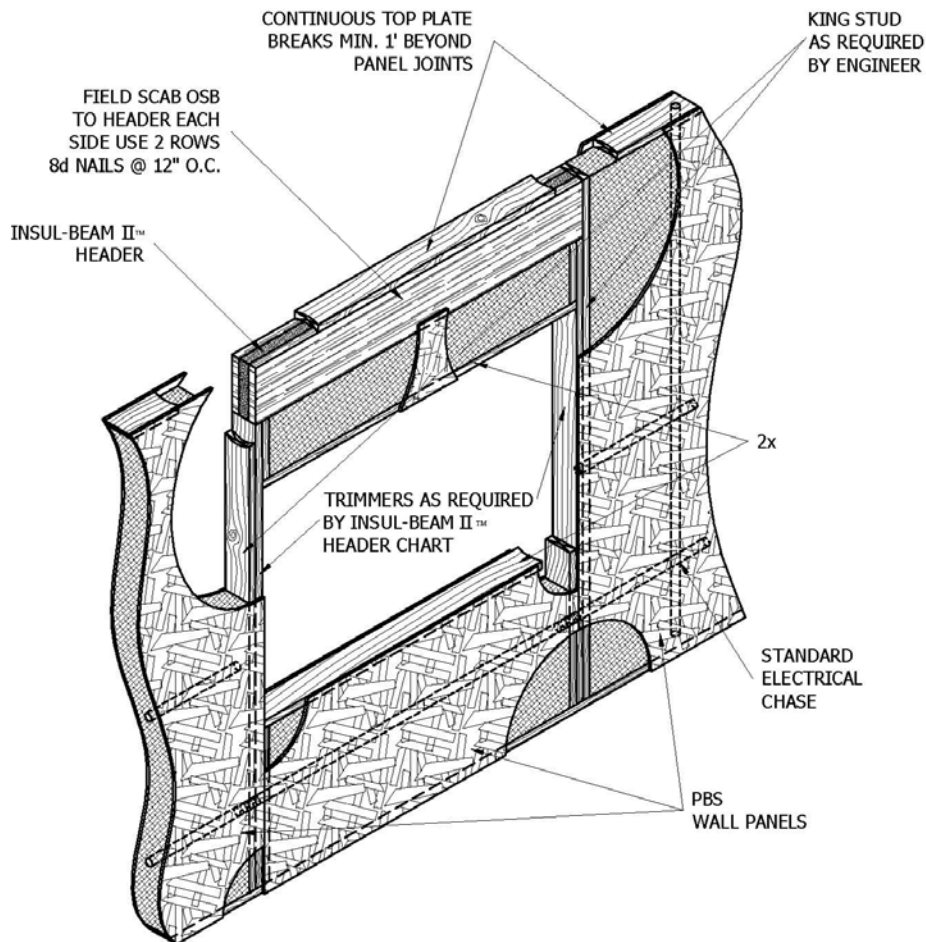
If the header is to be placed directly above the opening, a plate, the same width as the wall panel is nailed to the top of the header which will provide bearing for the OSB skins of the panel above the header. Detail PBS-211 depicts this condition.

For gable wall situations either of the previously described methods can be used for the header. If the header is placed directly below the top plate of the gable wall panel, the ends of the header will have to be plumb cut to match the slope of the wall.

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SEE DESIGN MANUAL FOR INSULBEAM II HEADER CHART

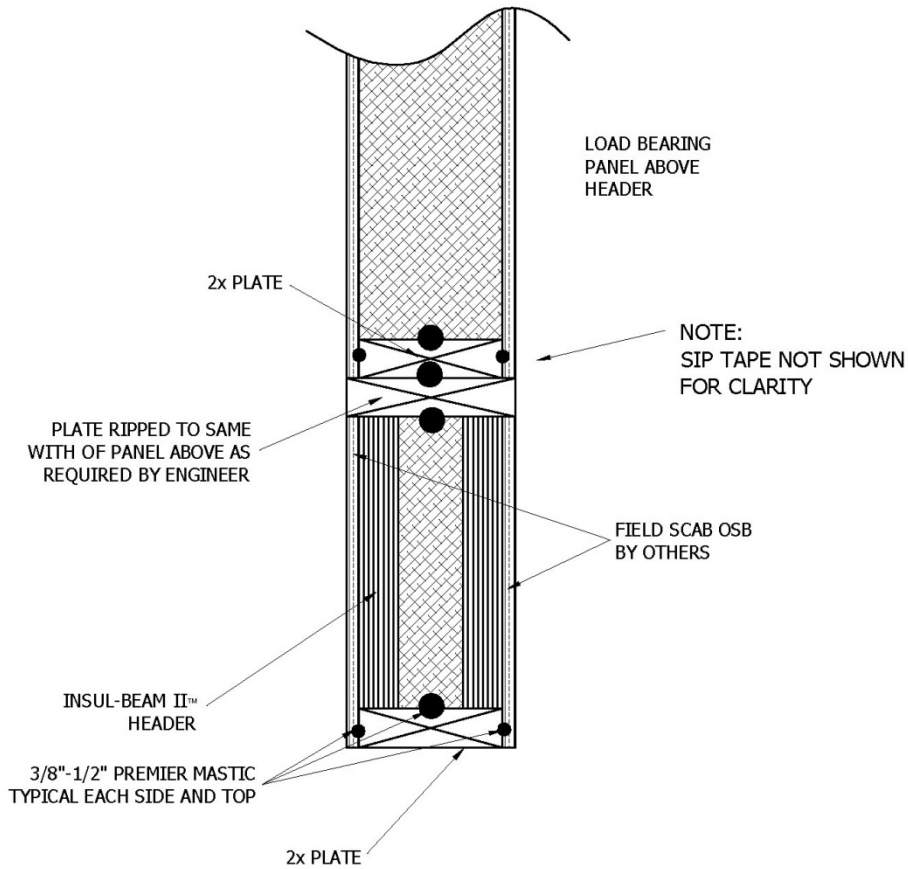


PBS-201 INSUL-BEAM HEADER 8-17-07
PREMIER BUILDING SYSTEMS

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SEE DESIGN MANUAL FOR INSULBEAM II HEADER CHART



INSUL-BEAM HEADER ABOVE OPENING

11-9-07

PREMIER BUILDING SYSTEMS

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LOW SLOPE COMMERCIAL ROOFING WITH PREMIER SIPs ROOF PANELS

Low slope commercial roofing with Premier SIPs is used in residential and commercial building applications. Commercial applications of Premier SIPs on a roof are typically low slope applications that require a contractor to have full understanding of code requirements.

Low slope roof applications typically utilize a single ply roofing membrane, built up roof (BUR) or modified bitumen as the roofing system. Within these systems are several techniques to secure the roof system to the panels. These include ballasted, adhered and mechanical attachment. Ballasted systems rely on rock or cementitious pavers as a weight to hold the membrane in place. Mechanical attachment is accomplished with the use of large screws through a membrane. Adhered systems use asphalt or adhesives that are placed on a substrate or carried on the membrane to adhere the membrane to the underlying deck. In some attached systems, the adhesive layer is applied to a board or sheet that has been mechanically attached to the deck.

When Premier SIPs are used as the deck on a low slope roof system, Premier SIPs recommends that a divorcement material be placed over the panels prior to the roof membrane. This divorcement can be a slip sheet on ballasted systems, a nailed base sheet on BUR systems and a cover board such as gypsum or wood fiber with adhered systems. These divorcement materials will minimize the effect of removing the roof membrane in the future, should it fail or need to be replaced. The panels require this protection since they need to remain intact to provide the structural capacities they were designed to support.

Further consideration needs to be given regarding the local building codes in effect and the architectural requirements of the roof assembly. Most jurisdictions in the United States follow the International Building Code (IBC) for commercial roof applications. Within the code is the requirement that the roof system meet a Class A, B or C designation based on ASTM E108 or UL 790 testing. When roof systems are placed over a Premier SIPs panel, a Class A, B or C rating needs to be determined for a combustible deck. In addition most architectural requirements for roof systems call out for a Class A roof system. The architect and roofing contractor need to be aware of the proposed roof membrane assembly to achieve a Class A rating over a combustible deck. Many times the easiest method to achieve the Class A requirement is to include a layer of gypsum board such as 1/4" DensDeck® over the panels. The attachment of this board needs to be sufficient to meet wind uplift requirements when used in conjunction with adhered membranes. In all cases the divorcement material should meet the requirements of the roofing membrane manufacturer.

When adhered systems are to be placed over Premier SIPs it is recommended that the membrane be attached with asphalt, pre applied pressure sensitive adhesives or water based adhesives. Solvent based adhesives could cause deterioration in the core of the Premier SIPs.

DensDeck® is a registered trademark of Georgia-Pacific.

Technical Bulletin #32b

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SEALING REQUIREMENTS FOR PANELS USED IN COMMERCIAL CONSTRUCTION

Premier SIPs are often used in commercial construction for floors, walls and or roofs. The proper use of vapor retarders and SIP Tape in these applications is a common question. The purpose of this technical bulletin is to provide guidelines for the use of vapor retarders, SIP Tape and panel mastic with Premier SIPs in commercial applications.

When installing Premier SIPs, the proper placement, as shown in the Premier SIPs details, of panel mastic at all panel joints is required. The function of the mastic is to provide a seal against air and vapor transmission.

The Building Codes view commercial construction in a different light than residential construction. In commercial construction, framed walls, floors and ceilings not ventilated to allow moisture to escape are required to have vapor retarders installed on the warm-in-winter side of the insulation. Commercial applications address ventilation through mechanical air handling and heat/cooling equipment. The key here is proper ventilation.

Commercial construction, typically, has a mechanical engineer involved with the design of the ventilation system. The mechanical engineer's design will take into account the amount of ventilation the structure requires based on the intended use of the building. In most applications this ventilation provides for numerous air changes which precludes the need for SIP tape or other vapor retarders. In addition, commercial structures intended to be used for storage or general warehouse do not need additional vapor control methods.

Buildings with intended uses involving pools, spas, or other high humidity conditions need to be looked at very carefully by the mechanical design professional with regard to adequate ventilation. In high humidity environments special attention to joint sealing and the use of SIP tape must be addressed.

In commercial construction that does not meet the ventilation requirements of the building code, Premier SIPs suggests that the IBC, as modified or approved by the local building code jurisdiction, be followed with regard to installing a vapor retarder.

If a vapor retarder is required in your commercial project, Premier SIPs recommends the use of SIP Tape over the panel joints. The SIP Tape is formulated with a permeance of less than 1. The APA has determined that OSB has a perm rating of less than 1. Since the OSB skins, of the panels that PBS produces, have a permeance rating of less than 1, the panel joint is the primary area of concern with a SIP system. The combination of the OSB skins and the SIP Tape meets the building code requirements for vapor retarders. Premier SIPs requires that panel mastic be used when joining panels.

Typically, 6" wide SIP Tape is used at all wall and roof panel joints as well as at wall panel corners. The connection of roof panels to exterior wall panels requires the use of 12" wide SIP Tape. Roof panels that have joints on supporting beams require 18" wide SIP Tape. A ridge beam is an example of this condition.

Please refer to the Premier SIPs typical details for illustrations of these conditions. The typical details can be requested by calling the number below, or it can be viewed online at www.premiersips.com.

Technical Bulletin #33c

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PREMIER SIPs USED AS SHEAR WALLS

Premier SIPs has recently completed the conversion of legacy evaluation reports PFC-5002 and NER-633 to ESR-1882. This conversion shows that Premier SIPs are in compliance with the 2006 International Building Code (IBC) and the 2006 International Residential Code (IRC).

A statement in the condition of use section of the ESR-1882 code report has been added by ICC-ES that did not appear in either PFC-5002 or NER-633. That statement is:

“When used as shear walls under the IBC or IRC, the panels are recognized for use in Seismic Design Categories A, B and C.”

The reason this statement appears in the report is that ICC-ES is in a quandary as to how to evaluate SIPs for use as shear walls in Seismic Zones D, E and F. As such, they have chosen not to evaluate SIPs for Zones D, E and F until they have clear, industry consensus, on the direction for testing requirements. According to ICC-ES this does not preclude the use of SIPs for shear walls in these seismic areas but rather engineering is required for the design.

The Insulfoam Technical Center has prepared this technical bulletin and a Technical Information Packet for use by code officials and engineers who have questions about using Premier SIPs as shear walls in seismic areas designated D, E and F.

The Technical Information Packet contains two test reports from the APA on cyclic shear wall testing conducted on Premier SIPs, and a comparative analysis from the APA on Premier SIPs and stick framed shear walls stating that the APA recommends PBS SIP shear walls should be designed with the same seismic design coefficients as light-frame walls sheathed with wood structural panels rated for shear resistance. Namely that the Response Modification Coefficient, $R = 6.5$; the System Over strength Factor, $\Omega_0 = 3$; and the Deflection Amplification Factor, $C_d = 4.0$. Also included in the Technical Information Packet is the detail PBS-005a to help clarify where to apply the mastic and SIP Tape in designed shear wall applications for seismic areas designated D, E and F.

A summary of the comparative analysis plots are shown on the following pages. The walls were tested following the Sequential Phase Displacement SPD protocol, which is clearly described in APA Reports T2003P-63 and T2004P-17. The hysteretic response of the walls can be seen in the following Figures 3-5. The hysteretic plots show a backbone curve, as well as an equivalent energy elastic-plastic (EEEP) curve, as defined by ASTM E-2126.

Please contact your Premier SIPs Sales Rep or the Technical Center to obtain your copy of the Technical Information Packet.

Technical Bulletin #33c

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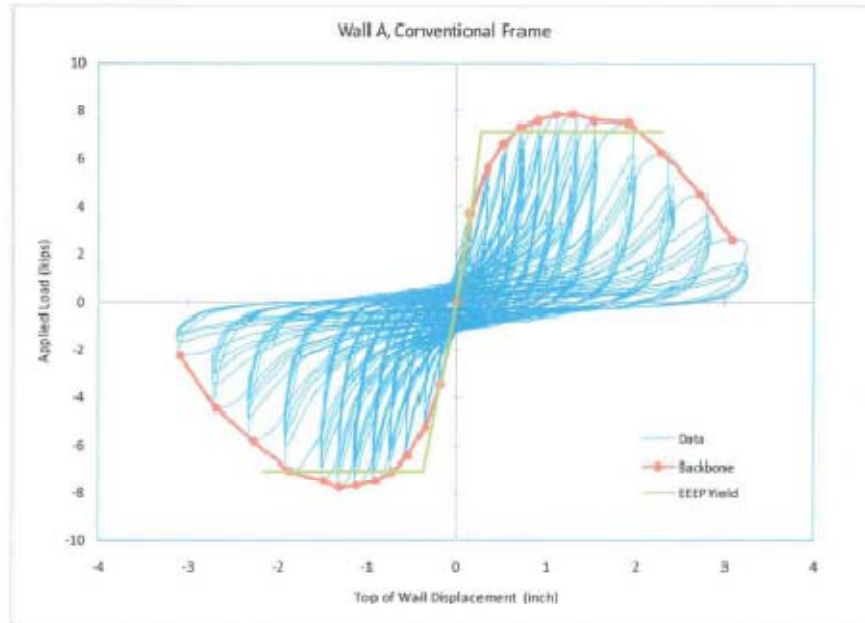


Figure 3. Cyclic response for conventionally framed wall.

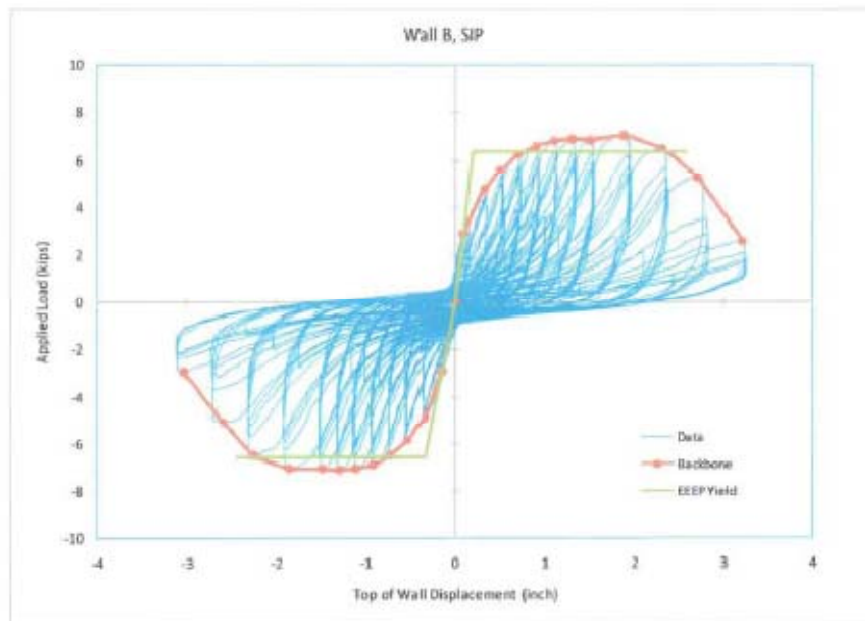


Figure 4. Cyclic response for SIPs wall.

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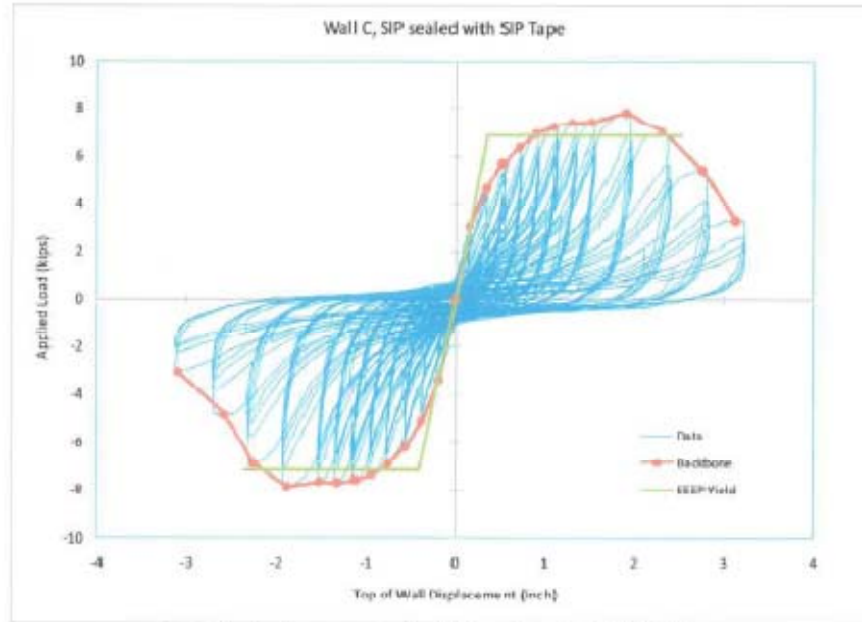


Figure 5. Cyclic response for SIPs wall sealed with SIP tape.

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ENERGY CALCULATIONS AND PREMIER SIPS

Energy efficiency is paramount in today's economy. Most everyone is concerned about conserving our natural resources and finding alternate sources of energy. Premier SIPS are helping Americans reduce energy use. Compared to traditional "stick built" construction, Premier SIPS save building owners up to 60% on monthly utility bills.

HVAC professionals are able to account for this energy efficiency in the design of the mechanical systems in Premier SIPS homes provided they have the proper information. Mechanical professionals use ACCA (Air Conditioning Contractors of America) Manual J as the design guide to calculate the requirements for the heating and cooling systems in our residential structures. Today, these calculations are computer based, but two important Premier SIPS properties need to be input into the software to provide meaningful results.

Manual J based calculations require the R-Value of the insulation material and the air infiltration rate, or air leakage rate. The R-Value is relatively straight forward. However, the air infiltration rate for Premier SIPS must be addressed properly. Design guidelines for Manual J calculations suggest a reasonable air leakage assumption between 0.35 to 0.50 natural air-changes per hour, unless a builder has data specific to their construction practices indicating they build tighter (or looser). This recommendation is for stick built homes.

Premier SIPS has blower door test data generated from homes using SIPS for the exterior walls and roof of homes that test out at .04 to .06 natural air changes per hour. These values for SIPS are on the order of 10 times better than what the Manual J design guidelines suggest. This reinforces what home owners have known for years about Premier SIPS energy efficiency.

Premier SIPS recommends that a value of .05 natural air changes per hour be used when performing Manual J heat loss calculations on homes using Premier SIPS as the exterior walls and roof. If the software being used does not allow for numerical input, select the tightest option.

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BREATHABLE ROOFING UNDERLAYMENT'S AND PREMIER SIPS

One of the many benefits of building with Premier SIPS is speed of construction. Speed of roof installation is especially beneficial in climates where precipitation is prevalent. However, precipitation during installation of roof panels and roofing materials should be properly addressed. The proper construction methodology and sequencing for the installation of roofing assemblies is to allow the OSB to dry adequately prior to the installation of the roofing underlayment.

When and if these conditions present themselves on your project, you may want to consider the use of a synthetic, breathable roofing underlayment as an alternative to traditional 15# or 30# roofing felts underneath the final roof covering. Breathable roofing underlayment's have perm ratings much greater than one. These materials allow water vapor to pass through the membrane yet restrict the bulk water movement back through the membrane toward the OSB skin of the SIP roof panel.

The idea behind this concept is to allow water that maybe trapped in the OSB to pass through the synthetic roofing underlayment as a vapor and once on the exterior side of the membrane it can eventually evaporate or condensate on the underside of the roofing material and run off the roof.

There are many manufactures of breathable underlayment's in North America. A quick internet search will turn up manufactures and suppliers available to supply your project. Be sure to check with the manufacture of the breathable underlayment for the perm rating of the underlayment and to see if there are any compatibility issues with asphalt shingles or the finished roof covering material you are using on your project.

Technical Bulletin #36b

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PREMIER SIPS – CONTINUOUS INSULATION SHEAR VALUE

Energy efficiency is paramount in building construction. Many local building codes are following the lead of ASHRAE and adopting requirements for continuous insulation (ci) over stud framed walls. Premier SIPS continuous insulation product is an answer to these local building code requirements.

Premier SIPS continuous insulation product consists of a layer of OSB laminated directly to an Insulfoam EPS insulation core. When the continuous insulation product is attached to the stud wall framing the OSB is held off the studs by the thickness of the EPS. This framing method varies from the typical application of OSB nailed directly to the stud framing. Questions about the racking shear capacity of this type of assembly have been raised by designers. The APA has published Technical Note 465E, APA Rated Siding Panels Over Rigid Foam Insulation Sheathing, which address this question for insulation thicknesses up to one inch.

Cyclic racking shear wall testing was conducted for applications using Insulfoam EPS insulation thickness of 1.5 inches. The assembly consisted of 7/16" Exposure 1 Oriented Strand Board (OSB) over 1.5 inches of Insulfoam EPS and nailed with 0.131 inch diameter x 3 1/4" nails driven by a pneumatic nail gun. The nails were driven through the OSB and foam and into the 2x4 studs behind. The 2x4 stud spacing was 24 inches on center. Nail spacing was 3 inches on center at the OSB edges, and 6 inches on center in the field of the OSB. The cyclic testing was conducted using the CUREE protocol according to AC 130. The average maximum load for the assembly was 557 plf. Designers can use this value with the appropriate safety factor to design walls utilizing this assembly.